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IN THE SPECIFICATION

Paragraph starting at page 3, line 24:

 To achieve the above-mentioned object, the present invention provides an amplifier circuit having a high time constant. An operational amplifier includes a non-<u>inverting</u> ~~converting~~ input terminal coupled to a ground, a <u>inverting</u> ~~converting~~ input terminal and an output terminal. A first resistor network including at least one stage is coupled between the <u>inverting</u> ~~converting~~ input terminal and the input terminal. Each stage of the first resistor network includes a first node, a first current path and a second current path connected to the first node. The first current path of each stage of the first resistor network is connected to the first node of the next stage, the second current path of each stage of the first resistor network is grounded, and the first current path of the first stage of the first resistor network is connected to the <u>inverting</u> ~~converting~~ input terminal. A loading unit is coupled between the <u>inverting</u> ~~converting~~ input terminal and the output terminal.

Paragraph starting at page 4, line 11:

 In addition, the present invention provides another amplifier circuit having a high time constant. An operational amplifier includes a non-<u>inverting</u> ~~converting~~ input terminal coupled to a ground, a <u>inverting</u> ~~converting~~ input terminal and an output terminal. A resistor network including a plurality of stages is connected between the <u>inverting</u> ~~converting~~ input terminal and the output terminal. Each stage of the resistor network includes a node, a first current path and a second current path connected to the node. The first current path of each stage of the resistor network is connected to the node of the next stage of the resistor network, the second current path of each stage resistor network is grounded, and the first current path of the last stage of the resistor network is connected to the <u>inverting</u> ~~converting~~ input terminal. A loading unit is coupled to the <u>inverting</u> ~~converting~~ input terminal.

Paragraph starting at page 6, line 23:

 FIG. 6~Fig. 8 are the diagrams of the amplifier circuits according to the embodiments of the present invention. The amplifier circuit comprises an operational amplifier 40 having a grounded non-<u>inverting</u> ~~converting~~ input terminal, a <u>inverting</u> ~~converting~~ input terminal coupled

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to the input voltage via a first resistor unit, and an output terminal coupled to the <u>inverting</u> ~~converting~~ input terminal via a second resistor unit. In the embodiments of the present invention, the first resistor unit, the second resistor unit, or both can be implemented by the resistor network disclosed in the present invention, as shown in FIG. 6, FIG. 7, and FIG. 8 respectively. If the resistor network comprises n stages, the resistance of the equivalent resistor is $R_{eq} = 2^N \times R$.

Paragraph starting at page 7, line 5:

FIG. 9 is a circuit showing the differentiator circuit according to the embodiment of the present invention, comprising an operational amplifier 40 having a grounded non-reverse input terminal, a <u>inverting</u> ~~converting~~ input terminal coupled to the input voltage via a capacitor C41, and an output terminal coupled to the <u>inverting</u> ~~converting~~ input terminal via a resistor unit. In the embodiment of the present invention, the resistor unit can be implemented by the resistor network disclosed in the present invention, as shown in FIG. 9. If the resistor network comprises n stages, the resistance of the equivalent resistor is $R_{eq} = 2^N \times R$.

Paragraph starting at page 7, line 15:

FIG. 10 is a circuit showing the integrator circuit according to the embodiment of the present invention, comprising an operational amplifier 40 having a grounded non-reverse input terminal, a <u>inverting</u> ~~converting~~ input terminal coupled to the input voltage via a resistor unit, and an output terminal coupled to the <u>inverting</u> ~~converting~~ input terminal via a capacitor C42. In the embodiment of the present invention, the resistor unit can be implemented by the resistor network disclosed in the present invention, as shown in FIG. 10. If the resistor network comprises n stages, the resistance of the equivalent resistor is $R_{eq} = 2^N \times R$.

Paragraph starting at page 7, line 25:

FIG. 11 is a circuit showing the low-pass filter circuit according to the embodiment of the present invention, comprising an operational amplifier 40 having a grounded non-reverse input terminal, a <u>inverting</u> ~~converting~~ input terminal coupled to the input voltage via a resistor R43, and an output terminal coupled to the <u>inverting</u> ~~converting~~ input terminal via a capacitor C43 and a resistor unit connected in parallel. In the embodiment of the present invention, the resistor unit

can be implemented by the resistor network disclosed in the present invention, as shown in FIG. 11. If the resistor network comprises n stages, the resistance of the equivalent resistor is $R_{eq} = 2^N \times R$.

Paragraph starting at page 8, line 6:

FIG. 12 is a circuit showing the high-pass filter circuit according to the embodiment of the present invention, comprising an operational amplifier 40 having a grounded non-reverse input terminal, a inverting ~~converting~~ input terminal coupled to the input voltage via a resistor unit and a capacitor C44 connected serially, and an output terminal coupled to the inverting ~~converting~~ input terminal via a resistor R44. In the embodiment of the present invention, the resistor unit can be implemented by the resistor network disclosed in the present invention, as shown in FIG. 12. If the resistor network comprises n stages, the resistance of the equivalent resistor is $R_{eq} = 2^N \times R$. The amplifier circuit, the differentiator, the integrator, the high-pass filter and the low-pass filter according to the embodiments of the present invention use the resistor network as resistive loading, so the equivalent resistance of the resistive loading is $R \cdot 2^N$, wherein N represents the stage number of the resistor network. Using resistor network comprising 16 stages as an example, the unit resistance is 0.024 Meg. In addition, the total resistance is only 1.176 Meg. Compared with conventional resistors, the resistor network requires only 1/1353 the resistance of the conventional resistor. Thus, the amplification factors of the amplifiers according to the embodiments of the present invention are more flexible by using the resistor network as the resistive loading. In addition, the differentiator, the integrator, the high-pass filter and the low-pass filter according to the embodiments of the present invention achieve higher time constant using the resistor network as the resistive loading.

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